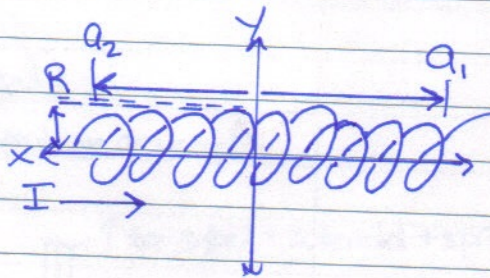


Seng 466
Solenoid Design
Logbook

1
March 10 2013

Mag field

$B = \frac{\mu_0 NI}{2R}$ (in center of loops)



$B(x) = \frac{\mu_0 NI}{2} \left(\frac{x - a_1}{\sqrt{(x - a_1)^2 + R^2}} - \frac{x - a_2}{\sqrt{(x - a_2)^2 + R^2}} \right)$ (Ttl field along x)

* if $L \gg 10R \rightarrow B = \mu_0 NI$

$\int E \cdot dA = \frac{Q}{\epsilon_0}$

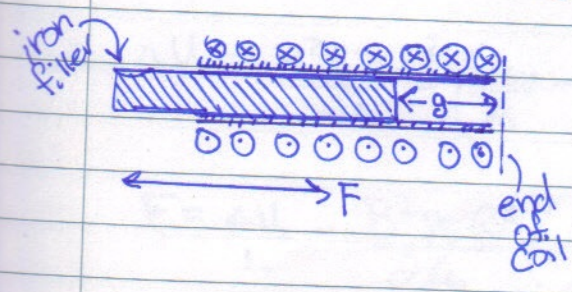
$\int B \cdot dA = \emptyset$

Force

$F = \frac{(F_m)^2 \mu_0 A}{(2g)^2} = \frac{(NI)^2 \mu_0 A}{(2g)^2}$

$A = \pi R^2$
 $g =$ gap from end of iron filler to end of coil

$F =$ Newtons
 $N =$ turns
 $I =$ Amps



March 11 2013

Solenoid Design

mass plunger = $\sim 5-10g$ = (steel)

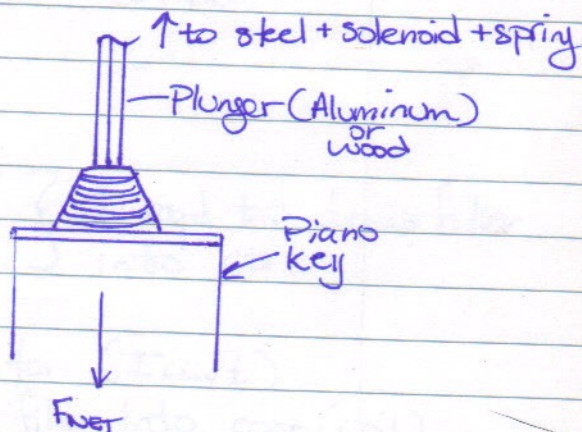
mass attachment = (Aluminum or wood)

Force to depress key = $0.65N$

$$\mu_{\text{steel}} = 8.75 \times 10^{-4}$$

$$\mu_{\text{iron}} = 4\pi \times 10^{-3} ?$$

$$\mu_{\text{copper}} = 1.0566 \times 10^{-6}$$



$$F_{\text{NET}} = F_{\text{key}} + F_{\text{spring}} - F_{\text{mass}}$$

$$F_{\text{NET}} = 0.65N$$

data from website: spiff.rit.edu... sol

$$U(\text{filled}) = (\text{Volume}) \frac{B^2}{2\mu_0} \left(\frac{\mu_m}{\mu_0} \right)$$

$$\text{Volume} = L\pi R^2$$

$$\Delta U = \frac{B^2 L \pi R^2}{2\mu_0} \left(\frac{\mu_m}{\mu_0} - 1 \right)$$

$$B = \mu_0 N I$$

$$F = \frac{\Delta U}{L} = \frac{B^2 \pi R^2}{2\mu_0} \left(\frac{\mu_m}{\mu_0} - 1 \right)$$

Test Dsgn

March 18 2013

Solenoid Length = 5cm
 Rad = 0.35cm (straw-optic)
 N = ~100 turns

~~filler~~

filler length = doesn't mtr (steel)
 mass = 5g
 Dia. =

(a) 30V \rightarrow ~0.2A ? } I reqd to draw filler
 5V \rightarrow ~0.88A } into coil.

\hookrightarrow 5V/0.88 w/o limiter (I limit)

\hookrightarrow effect: pulls steel filler into core (coil)
 and centers @ C.O.M. of steel

~~March 19 2013~~

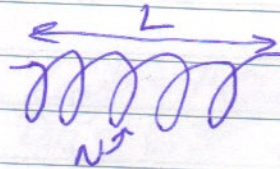
wrap page \rightarrow holding

~~max lifting = 133g @ 4.89A~~

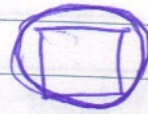
March 20
2013

Test Solenoid

20 Ga wire



18 turns in 15.93 mm

 $L = 119 \text{ mm}$

wound on square stock - Plastic

ID - $7.1 \times 7.1 \text{ mm}$ (square)
OD - $9.59 \text{ mm} \times 9.59 \text{ mm}$ (square)

Layers = 5

$$\frac{18 \text{ N}}{15.93 \text{ mm}} = 1.1299435$$

$$\frac{15.93 \text{ (mm)}}{18 \text{ (turns)}} = 0.885 \text{ ~~turns/mm~~ mm/turn}$$

$$\frac{N}{L} = 1.1299435 \text{ turns/mm}$$

$$1.1299435 \text{ turns/mm} \times 119 \text{ mm} = 134.463 \text{ turns}$$

$$\frac{134.463 \text{ turns}}{\text{layer}} \times 5 \text{ layers} = \boxed{672.3 \text{ turns}}$$

test solenoid

March 20 2013

mass steel = 34g length = 140.1mm
 Dia = 6.35mm (round)

max testing Current $I_{max} = 5A$

Ability to lift mass steel from vertical (opp g)
 @ 18.20 mm protruding into coil @ 5.2 A (I_{max})

(34g)
 lift mass inserted $\frac{1}{2}$ length (70.05mm) into
 coil @ $I = \sim 2A$ (1.9 \rightarrow 2.2) (friction)

$V = 5.37V_{ac}$
_{max}

March 21 2013

Max holding mass = 138g @ 4.88 A (5.37V_{ac})

Solenoid energy + Force

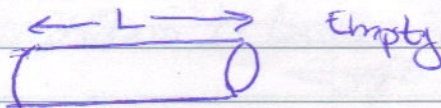
March 25 2013

$$U_{\text{empty}} = \frac{(L \pi R^2) B^2}{2 \mu_0}$$

U = Energy (J)

$$U_{\text{filled}} = \frac{(L \pi R^2) B^2}{2 \mu_0} \left(\frac{\mu_m}{\mu_0} \right)$$

$$F = \frac{\Delta U}{L}$$



$$U_{\text{empty}} = \frac{(19 \text{ mm } \pi \left(\frac{9.59 \text{ mm}}{2} \right)^2 B^2}{2 \mu_0}$$

$$L = 19 \text{ mm}$$

$$B = \mu_0 n I$$

$$R = 9.59 \text{ mm} / 2$$

$$U_{\text{empty}} = \frac{1.0349 \times 10^3 \text{ J}}{59.47 \times 10^{-6} \text{ J}}$$

$$n = 680$$

$$I = 4.88$$

L part-filled?



$$U_{\text{part-filled}} = \frac{V B^2}{2 \mu_0} \left(\frac{\mu_m}{\mu_0} \right)$$

$$V = 8.59555 \times 10^{-3} \text{ m}^3$$

$$= \frac{(L_2 \pi \left(\frac{9.59 \text{ mm}}{2} \right)^2) (680 \cdot 4.88 \cdot \mu_0)^2 \left(\frac{8.75 \times 10^{-4}}{\mu_0} \right)}{2 \mu_0}$$

$$U_{\text{pt}} = L_2 (347.986 \times 10^{-3}) \text{ J}$$

7

$$U_{\text{remain}} = L_3 \frac{(\pi \frac{9.59 \text{ mm}}{2})^2}{2 \mu_0} (680 - 4.88 \mu_0)^2 \quad \text{March 25 2013}$$

$$U_{\text{remain}} = L_3 (499.763 \times 10^{-6}) \text{ J}$$

$$U_{\text{empty}} = (U_{\text{pf}} + U_{\text{remain}}) =$$

$$(U_{\text{pf}} + U_{\text{remain}}) - U_{\text{empty}} = (L_2 (348 \times 10^{-3}) + L_3 (500 \times 10^{-6}))$$

$$= 59.47 \times 10^{-6}$$

$$U_{\text{filled}} = L \frac{(\pi \frac{9.59 \text{ mm}}{2})^2}{2 \mu_0} (680 - 4.88 \mu_0)^2 \left(\frac{\mu\text{m}}{\mu_0} \right)$$

$$U_{\text{filled}} = 41.41 \times 10^{-3} \text{ J}$$

$$U_{\text{filled}} - (U_{\text{pf}} + U_{\text{remain}}) = [L_2 = L_3 = \frac{1}{2} L]$$

$$\Delta U = 20.674 \times 10^{-3} \text{ J} \quad [\text{from bar } \frac{1}{2} L \text{ inserted}]$$

$$F = \frac{\Delta U}{L} = \frac{20.7 \times 10^{-3} \text{ J}}{119 \text{ mm} / 2} = 0.348 \text{ N}$$

[L/2 because 1/2 filled]

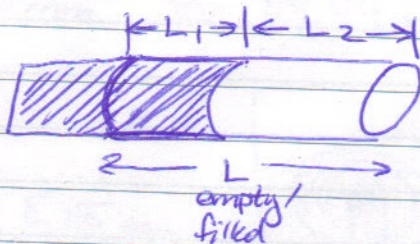
Actual test from 34g mass @ L/2 = 0.335 N

March 25 2013

Equation for Solenoid design

$$U_{\text{filled}} - (U_{\text{part-filled}} + U_{\text{remain}}) = \Delta U$$

$$\frac{\Delta U = F}{L_{\text{remain}}}$$



$$U_{\text{filled}} = (\text{Volume}) \frac{B^2}{2\mu_0} \left(\frac{\mu_m}{\mu_0} \right)$$

$$B = \mu_0 N I$$

$$\text{Vol} = \frac{L \pi R^2}{4}$$

$$U_{\text{part-filled}} = \frac{B^2}{2\mu_0} \left(\frac{\mu_m}{\mu_0} \right) (L_1 \pi R^2)$$

$$U_{\text{remain}} = \frac{L_2 \pi R^2 B^2}{2\mu_0}$$

March 27 2013

$$F_{\text{req}} (\text{to push piano key}) = 0.65 \text{ N}$$

$$F_{\text{spring}} (\text{holding mass up}) =$$

$$F_{\text{mass}} (\text{puncher}) =$$

$$\mu_m () =$$

$$L (\text{coil}) = 88.5 \text{ mm}$$

$$L_1 (\text{part fill}) =$$

$$L_2 (\text{remain empty}) =$$

$$\text{Radius (coil)} = \frac{14.29 \text{ mm}}{2} = 7.145 \text{ mm}$$

$$F_{\text{NET}} =$$

(key + spring - mass)

$$\text{mass} =$$

to be completed

Finished
final design

March 27 2013

turns:

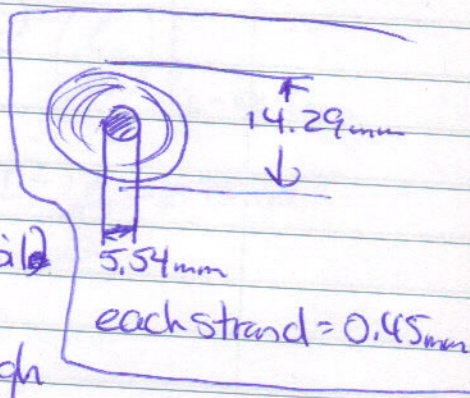
~15 turns / 7.85 mm for 84.44 mm (length)
~# Layers =

compensated for plug
(-4mm)

$$(14.29 - 5.54) \text{ mm} = 8.75 \text{ mm} \text{ (both sides)}$$

$$\frac{8.75}{2} = 4.375 \text{ mm (one side coil)}$$

$$\frac{4.375}{0.45 \text{ mm}} = 9.722 \text{ strands high}$$



Since packing is staggered (off max dia)
round up turns layers

$$\therefore \# \text{ Layers} = 10 \text{ layers}$$

$$\frac{15 \text{ t}}{7.85 \text{ mm}} = 1.910828 \frac{\text{t}}{\text{mm}}$$

$$1.9108 \frac{\text{t}}{\text{mm}} \times 84.44 \text{ mm} = 161.3503 \frac{\text{turns}}{\text{Layer}}$$

$$161.35 \frac{\text{turns}}{\text{Layer}} \times 10 \text{ Layers} = 1613.5 \text{ turns}$$

$$\therefore 1614 \text{ turns}$$

March 28 2013

$$F = \frac{\overset{\textcircled{1}}{U_{fill}} - (\overset{\textcircled{2}}{U_{pf}} + \overset{\textcircled{3}}{U_{rem}})}{\Delta L} \quad \left| \begin{array}{l} L = \\ L, x, L-x \end{array} \right.$$

$$\textcircled{1} \quad U_{fill} = \frac{L (\pi (7.145 \text{ mm})^2) (\frac{1600}{2})^2 \left(\frac{\mu m}{160}\right)}{2 \mu m} \quad \left| \begin{array}{l} L = 88.5 \text{ mm} \\ \mu m \end{array} \right.$$

$$= (88.5 \text{ mm}) (160.38 \times 10^{-6}) (1600^2) I^2 \frac{\mu m}{2} 8.75 \times 10^{-4}$$

$$\rightarrow U_{fill} = 15.897 \times 10^{-3} (I)^2 \text{ J}$$

$$\textcircled{2} \quad U_{pf} = x (160.38 \times 10^{-6}) (1600^2) I^2 \frac{8.75 \times 10^{-4}}{2}$$

$$\rightarrow U_{pf} = 179.627 \times 10^{-3} (x) (I^2) \text{ J}$$

$$\textcircled{3} \quad U_{remain} = (L-x) (160.38 \times 10^{-6}) (1600^2) I^2 \frac{8.75 \times 10^{-4}}{2}$$

$$\rightarrow U_{rem} = 179.627 \times 10^{-3} (L-x) (I^2) \text{ J} \quad \left| \begin{array}{l} L = 88.5 \text{ mm} \\ \mu m \end{array} \right.$$

$$F = \frac{\Delta U}{(L-x)} \quad \left[U_{rem} = (15.897 \times 10^{-3} - 179.627 \times 10^{-3} x) I^2 \text{ J} \right]$$